NOTE: SEE SHEET 2A FOR PLAN SHEET LAYOUT AT TIME OF INVESTIGATION

CONTENTS

LINE	STATION	PLAN	PROFILE	XSECT
-L-	13+90 - 39+50	4-5	7-9	12-17
-YI-	10+00 - 22+60	4,6	10-11	18-22

INVENTORY TEXT 3-3B DCP TEST RESULTS

STATE OF NORTH CAROLINA

DEPARTMENT OF TRANSPORTATION **DIVISION OF HIGHWAYS** GEOTECHNICAL ENGINEERING UNIT

ROADWAY SUBSURFACE INVESTIGATION

PROJ. REFERENCE NO. <u>41877.1.1 (W-5114)</u> F.A. PROJ. **STP-0068(10)** COUNTY <u>Guilford</u> PROJECT DESCRIPTION NC 68 from south of SR 2111 (East Harrell Road) to SR 4831 (Bartonshire Drive)

INVENTORY

STATE STATE PROJECT REFERENCE NO. N.C. W-5114 1

CAUTION NOTICE

THE SUBSURFACE INFORMATION AND THE SUBSURFACE INVESTIGATION ON WHICH IT IS BASED WERE MADE FOR THE PURPOSE OF STUDY, PLANNING, AND DESIGN, AND NOT FOR CONSTRUCTION OR PAY PURPOSES. THE VARIOUS FIELD BORING LOGS, ROCK CORES, AND SOIL TEST DATA AVAILABLE MAY BE REVIEWED OR INSPECTED IN RALEIGH BY CONTACTING THE N. C. DEPARTMENT OF TRANSPORTATION, GEOTECHNICAL ENGINEERING UNIT AT (1919) 707-6850, NEITHER THE SUBSURFACE PLANS AND REPORTS. NOR THE FIELD BORING LOGS. ROCK CORES. OR SOIL TEST DATA ARE PART OF THE CONTRACT.

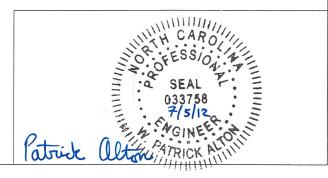
GENERAL SOIL AND ROCK STRATA DESCRIPTIONS AND INDICATED BOUNDARIES ARE BASED ON A GEMERAL SOIL AND ROCK STRATA DESCRIPTIONS AND INDICATED BOUNDARIES ARE BASED ON A COTOTECHNICAL INTERPRETATION OF ALL AVAILABLE SUBSURFACE DATA AND MAY NOT NECESSARILY REFLECT THE ACTUAL SUBSURFACE CONDITIONS BETWEEN BORNGS OR BETWEEN SAMPLED STRATA WITHIN THE BOREHOLE. THE LABORATORY SAMPLE DATA AND THE IN SITU (IN-PLACE) TEST DATA CAN BE RELIED ON DAILY TO THE DECREE OF RELIBBLITY INNERSTRATIN THE STANDARD TEST METHOD. THE OBSERVED WATER LEVELS OR SOIL MOISTURE CONDITIONS INDICATED IN THE SUBSURFACE INVESTIGATIONS ARE AS RECORDED AT THE TIME OF THE INVESTIGATION. THESE WATER LEVELS OR SOIL MOISTURE CONDITIONS MOICATED IN THE SUBSURFACE MOISTURE CONDITIONS MAY VARY CONSIDERABLY WITH TIME ACCORDING TO CLIMATIC CONDITIONS INCLUDING TEMPERATURES, PRECIPITATION, AND WIND, AS WELL AS OTHER NON-CLIMATIC FACTORS.

THE BIDDER OR CONTRACTOR IS CAUTIONED THAT DETAILS SHOWN ON THE SUBSUBFACE PLANS ARE PRELIMINARY ONLY AND IN MANY CASES THE FINAL DESIGN DETAILS ARE DEFERENT, FOR BIDDING AND CONSTRUCTION PURPOSES, REFER TO THE CONSTRUCTION PLANS AND DOCUMENTS FOR FINAL DESIGN INFORMATION ON THIS PROJECT. THE DEFARTMENT DOES NOT WARRANT OR GUARANTEE THE SUFFICIENCY OR ACCURACY OF THE INVESTIGATION MADE, NOR THE INTERPRETATIONS MADE, OR DINION OF THE DEPARTMENT AS TO THE TYPE OF MATERIALS AND CONDITIONS TO BE ENCOUNTERED. THE BIDDER OR CONTRACTOR IS CAUTIONED TO MAKE SUCH INDEPENDENT SUBSURFACE INVESTIGATIONS AS HE DEEMS NECESSARY TO SATISFY HUNSELF AS TO CONDITIONS TO BE ENCOUNTERED ON THIS PRODUCT. THE CONTRACTOR SHALL HAVE NO CLAIM FOR ADDITIONAL COMPENSATION OR FOR AN EXTENSION OF TIME FOR ANY REASON RESULTING FROM THE ACTUAL CONDITIONS ENCOUNTERED AT THE SITE DIFFERING FROM THOSE INDICATED IN THE SUBSURFACE INFORMATION.

LENSONNEL	
D. Racey	
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INVESTIGATED BY F&R, Inc.	_
CHECKED BY P. Alton, P.E.	

SUBMITTED BY__F&R, Inc.

DEDCOMME



DRAWN BY: D. Racey

NOTE - THE INFORMATION CONTAINED HEREIN IS NOT IMPLIED OR GUARANTEED BY THE N. C. DEPARTMENT OF TRANSPORTATION AS BEING ACCURATE NOR IT IS CONSIDERED TO BE PART OF THE PLANS, SPECIFICATIONS, OR CONTRACT FOR THE PROJECT.

NOTE - BY HAVING REQUESTED THIS INFORMATION THE CONTRACTOR SPECIFICALLY WAIVES ANY CLAIMS FOR INCREASED COMPENSATION OR EXTENSION OF TIME BASED ON DIFFERENCES BETWEEN THE CONDITIONS INDICATED HEREIN AND THE ACTUAL CONDITIONS AT THE PROJECT SITE.

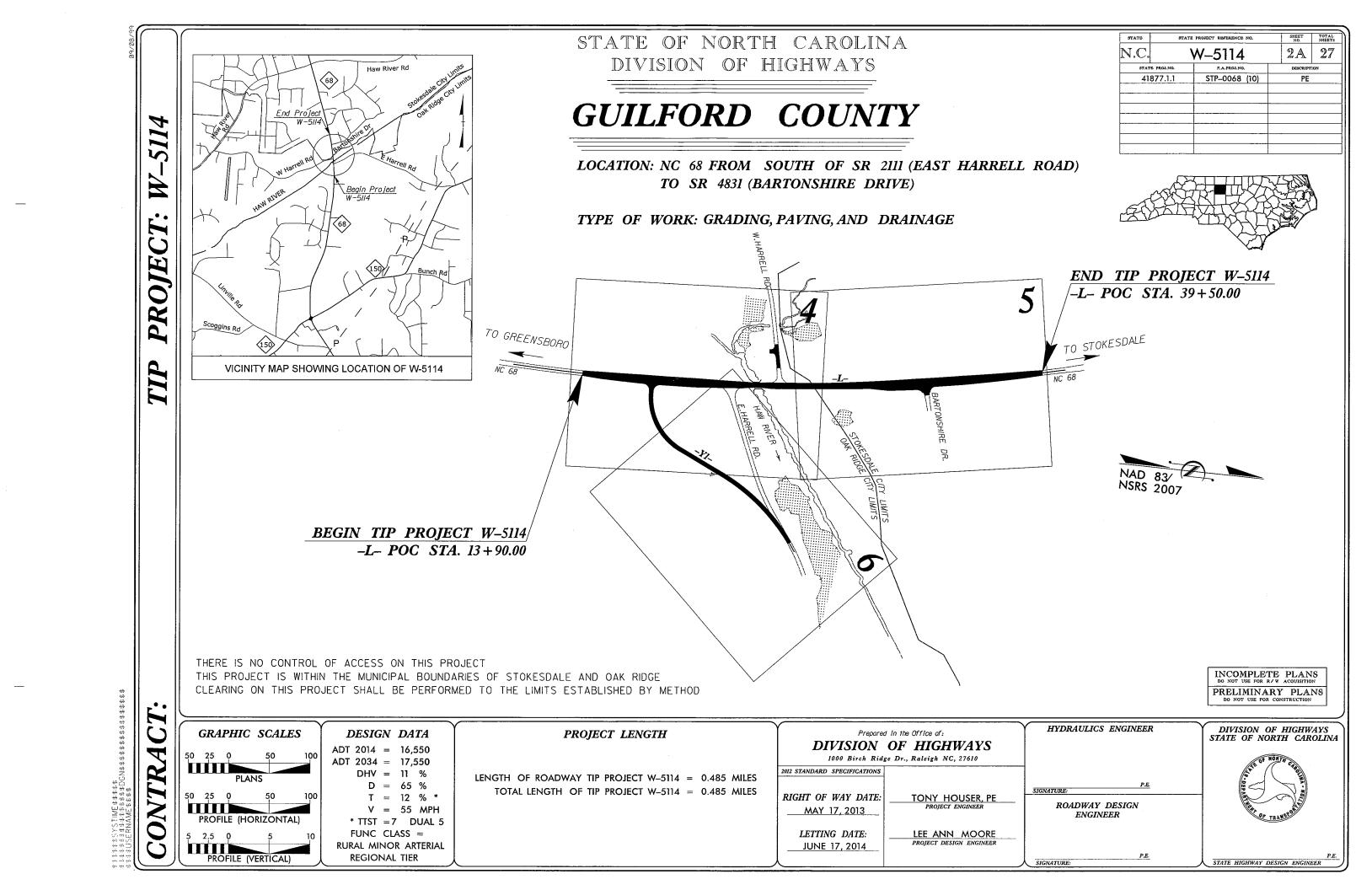
NORTH CAROLINA DEPARTMENT OF TRANSPORTATION

DIVISION OF HIGHWAYS

GEOTECHNICAL ENGINEERING UNIT

SUBSURFACE INVESTIGATION

			SOIL AND RO	CK LEGEND, TERM	s, symbol	S, AND ABBREVI	ATIONS	
	SOIL DESCRIPTION	T	GRADATION		L	ROCK	DESCRIPTION	TERMS AND DEFINITIONS
	INSOLIDATED, SEMI-CONSOLIDATED, OR WEATHERED EARTH MATERIALS	WELL GRADED - INDICATES A UNIFORM - INDICATES THAT S	GOOD REPRESENTATION OF PARTICLE SIZES IN SOIL PARTICLES ARE ALL APPROXIMATELY TH	FROM FINE TO COARSE. E SAME SIZE.(ALSO			T IF TESTED, WOULD YIELD SPT REFUSAL. AN INFERRED COASTAL PLAIN MATERIAL WOULD YIELD SPT REFUSAL.	ALLUVIUM (ALLUV.) - SOILS THAT HAVE BEEN TRANSPORTED BY WATER.
	NYINUOUS FLIGHT POWER AUGER, AND YIELD LESS THAN STANDARD PENETRATION TEST (AASHTO T206, ASTM D-1586). SOIL	POORLY GRADED)	IXTURE OF UNIFORM PARTICLES OF TWO OR		SPT REFUSAL IS	PENETRATION BY A SPLIT SPOON	SAMPLER EQUAL TO GR LESS THAN 0.1 FOOT PER 60 BLOW ON BETWEEN SOIL AND ROCK 1S OFTEN REPRESENTED BY A 2	
	SHTO SYSTEM, BASIC DESCRIPTIONS GENERALLY SHALL INCLUDE: RE.AASHTO CLASSIFICATION AND OTHER PERTINENT FACTORS SUCH		ANGULARITY OF GRAINS		OF WEATHERED I			AHENACEDUS - APPLIED TO ROCKS THAT HAVE BEEN DERIVED FROM SAND OR THAT CONTAIN SAND.
AS MINERALOGICAL COMPOSITION, ANGUL	LARITY, STRUCTURE, PLASTICITY, ETC. EXAMPLE:	THE ANGULARITY OR ROUNDNE SUBANGULAR, SUBROUNDED, OR	SS OF SOIL GRAINS IS DESIGNATED BY THE	TERMS: ANGULAR.	WEATHERED	BUMBUMA	LAIN MATERIAL THAT WOULD YIELD SPT N VALUES > 100	ARGILLACEOUS - APPLIED TO ALL ROCKS OR SUBSTANCES COMPOSED OF CLAY MINERALS, OR HAVING A NOTABLE PROPORTION OF CLAY IN THEIR COMPOSITION, AS SHALE, SLATE, ETC.
	CLAS MOIST WITH INTERBEDOED FINE SAND LAYERS, HIGHLY PLASTIC, A-7-6	SUBHINGULAN, SUBNOUNDED, UN	MINERALOGICAL COMPOSITION		ROCK (WR)	BLOWS PER FOO	T IF TESTED.	ARTESIAN - GROUND WATER THAT IS UNDER SUFFICIENT PRESSURE TO RISE ABOVE THE LEVEL
GENERAL GRANULAR MATER	ND AND AASHTO CLASSIFICATION RIALS SILT-CLAY MATERIALS ASSAULA MATERIALS	MINERAL NAMES SUCH AS QUAR	RTZ, FELDSPAR, MICA, TALC, KAOLIN, ETC. ARE 1		CRYSTALLINE ROCK (CR)		GRAIN IGNEOUS AND METAMORPHIC ROCK THAT PT REFUSAL IF TESTED, ROCK TYPE INCLUDES GRANITE.	AT WHICH IT IS ENCOUNTERED, BUT WHICH DOES NOT NECESSARILY RISE TO OR ABOVE THE GROUND SURFACE.
CLASS. (≤ 35% PASSING	*200) (> 35% PASSING *200) UNGANIC MATERIALS	WHENEVER THEY ARE CONSIDER	RED OF SIGNIFICANCE.			GNEISS, GABBRO,		CALCAREOUS (CALC.) - SOILS THAT CONTAIN APPRECIABLE AMOUNTS OF CALCIUM CARBONATE.
GROUP A-1 A-3 CLASS. A-1-a A-1-b A-2-4 A	A-2		COMPRESSIBILITY		NON-CRYSTALLINE ROCK (NCR)	SEDIMENTARY RO	OCK THAT WOULD YELLD SPT REFUSAL IF TESTED. ROCK TYP	COLLUYIUM - ROCK FRAGMENTS MIXED WITH SOIL DEPOSITED BY GRAVITY ON SLOPE OR AT BOTTOM OF SLOPE,
SYMBOL 000000000000000000000000000000000000	1-2-5 A-2-6 A-2-7 A-3 A-6, A-7	SLIGHTLY COMPRESS MODERATELY COMPR	ESSIBLE LIQUID LIMIT	LESS THAN 31 EOUAL TO 31-50	COASTAL PLAIN	COASTAL PLAIN	ITE, SLATE, SANDSTONE, ETC. SEDIMENTS CEMENTED INTO ROCK, BUT MAY NOT YIELD	CORE RECOVERY (REC.) - TOTAL LENGTH OF ALL MATERIAL RECOVERED IN THE CORE BARREL DIVIDED BY TOTAL
% PASSING		HIGHLY COMPRESSIB	PERCENTAGE OF MATERIA	GREATER THAN 50	SEDIMENTARY ROCK (CP)	SPT REFUSAL, R	OCK TYPE INCLUDES LIMESTONE, SANDSTONE, CEMENTED	LENGTH OF CORE RUN AND EXPRESSED AS A PERCENTAGE.
# 10 50 MX	GRANULAR SILT- MUCK,	ORGANIC MATERIAL	GRANULAR SILT - CLAY			WE.	ATHERING	<u>DIKE</u> - A TABULAR BODY OF IGNEOUS ROCK THAT CUTS ACROSS THE STRUCTURE OF ADJACENT ROCKS OR CUTS MASSIVE ROCK.
# 40 30 MX 50 MX 51 MN # 200 15 MX 25 MX 10 MX 35 MX 3	35 MX 35 MX 36 MN 36 MN 36 MN 36 MN 36 MN	TRACE OF ORGANIC MATTER	SOILS SOILS 2 - 3% 3 - 5% TR	OTHER MATERIAL ACE 1 - 10%			DINTS MAY SHOW SLIGHT STAINING. ROCK RINGS UNDER	DIP - THE ANGLE AT WHICH A STRATUM OR ANY PLANAR FEATURE IS INCLINED FROM THE
1000 4107		LITTLE ORGANIC MATTER MODERATELY ORGANIC	3 - 5% 5 - 12% LIT	TLE 10 - 20%	1	MER IF CRYSTALLINE. K GENERALLY FRESH JOINTS STAIN	ED, SOME JOINTS MAY SHOW THIN CLAY COATINGS IF OPEN,	HORIZONTAL.
	8 MX II MN II MN II MX II MN II MN LITTLE OR HIGHLY	HIGHLY ORGANIC		ME 20 - 35% GHLY 35% AND ABOVE	(V SLI.) CRYS	STALS ON A BROKEN SPECIMEN FAC	E SHINE BRIGHTLY, ROCK RINGS UNDER HAMMER BLOWS IF	DIP DIRECTION (DIP AZIMUTH) - THE DIRECTION OR BEARING OF THE HORIZONTAL TRACE OF THE LINE OF DIP, MEASURED CLOCKWISE FROM NORTH.
GROUP INDEX Ø Ø Ø			GROUND WATER			A CRYSTALLINE NATURE. < GENERALLY FRESH. JOINTS STAIN	ED AND DISCOLORATION EXTENDS INTO ROCK UP TO	FAULT - A FRACTURE OR FRACTURE ZONE ALONG WHICH THERE HAS BEEN DISPLACEMENT OF THE SIDES RELATIVE TO ONE ANOTHER PARALLEL TO THE FRACTURE.
	Y OR CLAYEY SILTY CLAYEY ORGANIC		EVEL IN BORE HOLE IMMEDIATELY AFTER (DRILLING	(SL1.) 1 INC		AY. IN GRANITOID ROCKS SOME OCCASIONAL FELOSPAR CRYSTALLINE ROCKS RING UNDER HAMMER BLOWS.	FISSILE - A PROPERTY OF SPLITTING ALONG CLOSELY SPACED PARALLEL PLANES.
MATERIALS SAND SAND GRAVE	EL AND SAND SOILS SOILS MATTER	4	VATER LEVEL AFTER 24 HOURS				DISCOLORATION AND WEATHERING EFFECTS. IN	FLOAT - ROCK FRAGMENTS ON SURFACE NEAR THEIR ORIGINAL POSITION AND DISLODGED FROM
GEN. RATING AS A EXCELLENT TO G	SOOD FAIR TO POOR FAIR TO POOR UNSUITABLE	V PW PERCHED	WATER, SATURATED ZONE, OR WATER BEAR!	NG STRATA	(MOD.) GRAN		E DULL AND DISCOLORED, SOME SHOW CLAY, ROCK HAS D SHOWS SIGNIFICANT LOSS OF STRENGTH AS COMPARED	PARENT MATERIAL.
SUBGRADE DI OF A 7 F SUBGRADE I	S ≤ LL - 30 : PI OF A-7-6 SUBGROUP IS > LL - 30	SPRING O	IR SEEP		HTIW	FRESH ROCK.		<u>FLOOD PLAIN (FP)</u> - LAND BORDERING A STREAM, BUILT OF SEDIMENTS DEPOSITED BY THE STREAM.
	NSISTENCY OR DENSENESS	,	MISCELLANEOUS SYMBOLS	<u> </u>			I OR STAINED. IN GRANITOID ROCKS, ALL FELDSPARS DULL W KAOLINIZATION. ROCK SHOWS SEVERE LOSS OF STRENGTH	FORMATION (FM.) - A MAPPABLE GEOLOGIC UNIT THAT CAN BE RECOGNIZED AND TRACED IN
	TNESS OR RANGE OF STANDARD RANGE OF UNCONFINED COMPRESSIVE STRENGTH	T ROADWAY EMBANK			(MOD. SEV.) AND		GIST'S PICK. ROCK GIVES CLUNK SOUND WHEN STRUCK.	THE FIELD.
CONSIS	STENCY (N-VALUE) COMPRESSIVE STRENGTH (N-VALUE) (TONS/FT ²)	WITH SOIL DESCR		W/ CORE	1		OR STAINED ROCK FABRIC CLEAR AND EVIDENT BUT REDUC	JOINT - FRACTURE IN ROCK ALONG WHICH NO APPRECIABLE MOVEMENT HAS OCCURRED.
GENERALLY VERY L		SOIL SYMBOL	AUGER BORING	— SPT N-YALUE	(SEV.) IN S		NITOID ROCKS ALL FELOSPARS ARE KAOLINIZED TO SOME	LEGGE - A SHELF-LIKE RIDGE OR PROJECTION OF ROCK WHOSE THICKNESS IS SMALL COMPARED TO ITS LATERAL EXTENT.
MATERIAL MEDIUM	1 DENSE 10 TO 30 N/A	ARTIFICIAL FILL		(REF)— SPT REFUSAL		TESTED, YIELDS SPT N VALUES > 18		LENS - A BODY OF SOIL OR ROCK THAT THINS OUT IN ONE OR MORE DIRECTIONS.
(NON-COHESIVE) DENS		THAN ROADWAY E		•			OR STAINED, ROCK FABRIC ELEMENTS ARE DISCERNIBLE BU	MOTTLED (MOT.) - IRREGULARLY MARKED WITH SPOTS OF DIFFERENT COLORS, MOTTLING IN SOILS USUALLY INDICATES POOR AERATION AND LACK OF GOOD DRAINAGE.
VERY S		- INFERRED SOIL B		LL	REMA	AINING. SAPROLITE IS AN EXAMPLE	O SOIL STATUS, WITH ONLY FRAGMENTS OF STRONG ROCK OF ROCK WEATHERED TO A DEGREE SUCH THAT ONLY MIND	PERCHED WATER - WATER MAINTAINED ABOVE THE NORMAL GROUND WATER LEVEL BY THE PRESENCE OF AN
GENERALLY SOFT SILT-CLAY MEDIUM	T 2 TO 4 0.25 TO 0.50	INFERRED ROCK L	INE A PIEZOMETER INSTALLATION				RIC REMAIN. IF TESTED, YIELDS SPT N VALUES < 100 BPF	INTERVENING IMPERVIOUS STRATUM.
MATERIAL STIF	F 8 TO 15 1 TO 2	TTTT ALLUVIAL SOIL B	OUNDARY SLOPE INDICATO	DR .			NOT DISCERNIBLE.OR DISCERNIBLE ONLY IN SMALL AND MAY BE PRESENT AS DIKES OR STRINGERS. SAPROLITE IS	RESIDUAL (RES.) SOIL - SOIL FORMED IN PLACE BY THE WEATHERING OF ROCK, ROCK QUALITY DESIGNATION (RQD) - A MEASURE OF ROCK QUALITY DESCRIBED BY TOTAL LENGTH OF
(COHESIVE) VERY S HARD		25/025 DIP & DIP DIRECT	TION OF INSTALLATION		ALSO	AN EXAMPLE.		MOCK SEGMENTS EQUAL TO OR GREATER THAN 4 INCHES DIVIDED BY THE TOTAL LENGTH OF CORE RUN AND
Tı	EXTURE OR GRAIN SIZE	ROCK STRUCTURES	S 🛆 CONE PENETROM	ETER TEST		· · · · -	HARDNESS	EXPRESSED AS A PERCENTAGE. SAPROLITE (SAP.) - RESIDUAL SOIL THAT RETAINS THE RELIC STRUCTURE OR FABRIC OF THE
U.S. STD. SIEVE SIZE	4 10 40 60 200 270		SOUNDING ROD			NOT BE SCRATCHED BY KNIFE OR FERAL HARD BLOWS OF THE GEOLOG	SHARP PICK. BREAKING OF HAND SPECIMENS REQUIRES	PARENT ROCK.
OPENING (MM)	4.76 2.00 0.42 0.25 0.075 0.053		ABBREVIATIONS				K ONLY WITH DIFFICULTY. HARD HAMMER BLOWS REQUIRED	SILL - AN INTRUSIVE BODY OF IGNEOUS ROCK OF APPROXIMATELY UNIFORM THICKNESS AND RELATIVELY THIN COMPARED WITH ITS LATERAL EXTENT, THAT HAS BEEN EMPLACED PARALLEL
	GRAVEL COARSE FINE SILT CLAY	AR - AUGER REFUSAL	MICA MICACEOUS	VST - VANE SHEAR TEST		DETACH HAND SPECIMEN.		TO THE BEDDING OR SCHISTOSITY OF THE INTRUDED ROCKS.
(BLOR,) (COB.)	(GR.) (CSE. SD.) (F SD.) (SL.) (CL.)	BT - BORING TERMINATED CL CLAY	MOD MODERATELY ND - NOT DETERMINED	WEA WEATHERED			K. GOUGES OR GROOVES TO 0.25 INCHES DEEP CAN BE LOGIST'S PICK. HAND SPECIMENS CAN BE DETACHED	SLICKENSIDE - POLISHED AND STRIATED SURFACE THAT RESULTS FROM FRICTION ALONG A FAULT OR SLIP PLANE.
GRAIN MM 305 75 SIZE IN 12 3	2.0 0.25 0.05 0.005	CPT - CONE PENETRATION	TEST NP - NON PLASTIC	7 - DRY UNIT WEIGHT		MODERATE BLOWS.	CHEC DEED BY CIGN DOLCCUDE OF WHICE OF DICK DOLLY	STANDARD PENETRATION TEST (PENETRATION RESISTANCE) (SPT) - NUMBER OF BLOWS (N OR BPF) OF
	TURE - CORRELATION OF TERMS	CSE COARSE DMT - DILATOMETER TEST	NT - NOT TESTED ORG ORGANIC	SAMPLE ABBREVIATIONS	HARD CAN	N BE EXCAVATED IN SMALL CHIPS	CHES DEEP BY FIRM PRESSURE OF KNIFE OR PICK POINT. TO PEICES 1 INCH MAXIMUM SIZE BY HARD BLOWS OF THE	A 140 LB. HAMMER FALLING 30 INCHES REQUIRED TO PRODUCE A PENETRATION OF 1 FOOT INTO SOIL WITH A 2 INCH OUTSIDE DIAMETER SPLIT SPOON SAMPLER, SPT REFUSAL IS PENETRATION EQUAL TO OR LESS
SOIL MOISTURE SCALE	FIELD MOISTURE CHIDE FOR FIELD MOISTURE DESCRIPTION	e - VOID RATIO F - FINE	ROWY. EMBANK ROADWAY EMBANKMENT	S - BULK SS - SPLIT SPOON		NT OF A GEOLOGIST'S PICK.	BY KNIFE OR PICK. CAN BE EXCAVATED IN FRAGMENTS	THAN 0.1 FOOT PER 60 BLOWS.
(ATTERBERG LIMITS)	DESCRIPTION SOLDE TON TIEED POISTONE SESSINI TION	FIAD-FILLED IMMEDIATELY A	FTER DRILLING SAP SAPROLITIC	ST - SHELBY TUBE	FRO	DM CHIPS TO SEVERAL INCHES IN S	SIZE BY MODERATE BLOWS OF A PICK POINT. SMALL, THIN	STRATA CORE RECOVERY (SREC.) - TOTAL LENGTH OF STRATA MATERIAL RECOVERED DIVIDED BY TOTAL LENGTH OF STRATUM AND EXPRESSED AS A PERCENTAGE.
	- SATURATED - USUALLY LIQUID; VERY WET, USUALLY (SAT.) FROM BELOW THE GROUND WATER TABLE	FRAC FRACTURED, FRACTU FRAGS FRAGMENTS	JRES SD SAND, SANDY SL SILT, SILTY	RS - ROCK RT - RECOMPACTED TRIAXIAL		CES CAN BE BROKEN BY FINGER PR	RESSURE. EXCAVATED READILY WITH POINT OF PICK, PIECES I INCH	STRATA ROCK QUALITY DESIGNATION (SROD) - A MEASURE OF ROCK QUALITY DESCRIBED BY
LL LIQUID LIMIT	CSHI, PROP BELOW THE GROUND WHIEN THOLE	HI HIGHLY	SLI SLIGHTLY w - MOISTURE CONTENT	CBR - CALIFORNIA BEARING	SOFT OR	MORE IN THICKNESS CAN BE BROKE	EN BY FINGER PRESSURE. CAN BE SCRATCHED READILY BY	TOTAL LENGTH OF ROCK SEGMENTS WITHIN A STRATUM EQUAL TO OR GREATER THAN 4 INCHES DIVIDED BY THE TOTAL LENGTH OF STRATA AND EXPRESSED AS A PERCENTAGE.
PLASTIC RANGE <	- WET - (W) SEMISOLID: REQUIRES DRYING TO	MED MEDIUM	IPMENT USED ON SUBJECT F	PROJECT	4	GERNAIL. TURE SPACING	BEDDING	TOPSOIL (TS.) - SURFACE SOILS USUALLY CONTAINING ORGANIC MATTER.
(PI) PL PLASTIC LIMIT	ATTAIN OPTIMUM MOISTURE		1	HAMMER TYPE:	TERM	SPACING	TERM THICKNESS	BENCH MARK:
OPTIMUM MOISTURE	- MOIST - (M) SOLID; AT OR NEAR OPTIMUM MOISTURE	DRILL UNITS:	ADVANCING TOOLS:	X AUTOMATIC MANUAL	VERY WIDE	MORE THAN 10 FEET	VERY THICKLY BEDDED > 4 FEET THICKLY BEDDED 1.5 - 4 FEET	TBM 1: BL-10 N: 893,336.8225 E: 1,709,189,5301 ELEV. = 826.73 FT.
OM OPTIMUM MOISTURE SL SHRINKAGE LIMIT		MOBILE B	CLAY BITS		WIDE MODERATELY CL	3 TO 10 FEET LOSE 1 TO 3 FEET	THINLY BEDDED Ø.16 - 1.5 FEET	TBM 2: BL-9 N: 892,173.9430 E: 1,709,317.6907 ELEV. = 805.89 FT.
	- DRY - (D) ATTAIN DETINING MOTERUPE		6' CONTINUOUS FLIGHT AUGER	CORE SIZE:	CLOSE VERY CLOSE	0.16 TO 1 FEET LESS THAN 0.16 FEET	VERY THINLY BEDOED 0.03 - 0.16 FEET THICKLY LAMINATED 0.008 - 0.03 FEET	NOTES:
	HITHIN OF THOM MOISTONE	BK-51	X 8' HOLLOW AUGERS				THINLY LAMINATED < 0.008 FEET	
	PLASTICITY PLASTICITY PROPERTY	CME-45C	HARD FACED FINGER BITS		FOR SEDIMENTARY F		NG OF THE MATERIAL BY CEMENTING, HEAT, PRESSURE, ETC.	
NONPLASTIC	PLASTICITY INDEX (PI) ORY STRENGTH 0-5 VERY LOW	X CME-55	TUNGCARBIDE INSERTS			DUDDING	WITH FINGER FREES NUMEROUS GRAINS;	·
LOW PLASTICITY MED. PLASTICITY	6-15 SLIGHT 16-25 MEDIUM		CASING W/ ADVANCER	HAND TOOLS:	FRIABLE		BLOW BY HAMMER DISINTEGRATES SAMPLE.	
HIGH PLASTICITY	26 GR MORE HIGH	PORTABLE HOIST	TRICONE STEEL TEETH	POST HOLE DIGGER	MODERAT		CAN BE SEPARATED FROM SAMPLE WITH STEEL PROBE: EASILY WHEN HIT WITH HAMMER.	
	COLOR		TRICONE TUNGCARB.	X HAND AUGER/DCP	INDURATE		ARE DIFFICULT TO SEPARATE WITH STEEL PROBE:	
DESCRIPTIONS MAY INCLUDE COLOR	OR COLOR COMBINATIONS (TAN, RED, YELLOW-BROWN, BLUE-GRAY).		CORE BIT	SOUNDING ROD VANE SHEAR TEST	INDURIE		T TO BREAK WITH HAMMER.	
MODIFIERS SUCH AS LIGHT, DAR	K. STREAKED. ETC. ARE USED TO DESCRIBE APPEARANCE.	Ш	LI		EXTREME		AMMER BLOWS REQUIRED TO BREAK SAMPLE:	
		1	<u> </u>		l	SAMPLE	BREAKS ACROSS GRAINS.	





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July 5, 2012

State Project No.:

41877.1.1

TIP No.:

W-5114

F.A. Number:

STP-0068 (10)

County:

Guilford

Description:

NC 68 from south of SR 2111 (East Harrell Road) to SR 4831 (Bartonshire

Drive) in Oak Ridge and Stokesdale

SUBJECT:

Geotechnical Report – Inventory

Project Description

This project involves widening existing NC 68 (-L-) for a distance of 0.48 miles and the realignment of East Harrell Road (-Y1-) for a distance of 0.24 miles in the towns of Oak Ridge and Stokesdale, North Carolina. NC 68 is proposed to be widened for safety improvements with the addition of paved shoulders and medians along the existing 2-lane roadway. The widening begins approximately 800 feet south of East Harrell Road and ends approximately 650 feet north of Bartonshire Drive, and extends through an area that contains residences and undeveloped wooded property throughout its entire length. Proposed fills are generally less than 6 or 7 feet in height while proposed cuts are generally less than 4 or 5 feet in height with the exception of the southern end of the project where the maximum cut is approximately 13 feet in height.

The realignment of East Harrell Road begins at NC 68 approximately 450 feet south of the road's current intersection with NC 68 and intersects existing East Harrell Road approximately 1000 feet east of NC 68. Maximum cut and fill heights are approximately 28 feet and 9 feet, respectively.

The geotechnical field investigation was performed between April 16 and 24 of 2012. Eight standard penetration test (SPT) borings were advanced with an ATV-mounted CME-55 drill rig with an automatic hammer. In addition, six shallow hand auger borings were also completed in areas of minimal fill or in areas that were inaccessible to our drill rig. Dynamic cone penetrometer (DCP) testing was performed in all of the hand auger borings in general accordance with ASTM Special Technical Publication No. 399. The number of blows required to drive the 1.375-inch diameter steel cone three consecutive 1.75-inch

increments is recorded and the blows of the last two 1.75-inch increments are averaged to obtain the DCP N_c -values, representing the penetration resistance of the soil. Representative soil samples were collected for visual classification in the field and for laboratory analysis by F&R's soil testing laboratory.

The following alignments were investigated:

<u>Line</u>	<u>Station(±)</u>
-L-	13+90 to 39+50
-Y1-	10+00 to 22+60

Areas of Special Geotechnical Interest

1) <u>Crystalline Rock</u>: The following locations were found to contain crystalline rock within 6 feet of the proposed grade:

<u>Line</u>	<u>Station(±)</u>
-Y1-	11+50, 100' right
-Y1-	19+50, 25' right

2) <u>Weathered Rock</u>: The following locations were found to contain weathered rock above or within 6 feet of the proposed grade that have a potential to require ripping or blasting for removal:

<u>Line</u>	<u>Station (±)</u>
-Y1-	11+50
-Y1-	17+50, 25' right
-Y1-	19+42, 14' left
-Y1-	19+50, 25' right

3) <u>Hand Auger Refusal</u>: Hand auger refusal was achieved at the following locations which may be an indication of the presence of very dense or hard soils, but may also be an indication of the presence of weathered rock and/or crystalline rock:

<u>Line</u>	Station (±)
-L-	17+00, 50' left
-L-	17+05, 50' left
-L-	17+77, 22' right
-L-	35+00, 29' right
-L-	35+07, 35' right

4) Groundwater: The following location exhibited groundwater within 6 feet of the proposed grade:

<u>Line</u> <u>Station (±)</u>
-L- 27+00, 35' right

Although stabilized groundwater was not encountered at the borings located at -L- 23+00 and -L- 24+17, wet and/or saturated soils were encountered and could be an indication of the presence of or potential for shallow groundwater.

5) <u>Highly Plastic Soils</u>: The following location was found to contain highly plastic soils within the upper 3 feet of proposed grade which have the potential for subgrade instability during construction:

<u>Line</u> <u>Station (±)</u> -L- 31+00, 28' left

6) Organic Soils: The following location was found to contain loose and moderately organic soils, which have the potential for subgrade instability during construction:

<u>Line</u> <u>Station (±)</u> -L- 35+00, 29' right

Physiography and Geology

The project is located in the Piedmont Physiographic Province of North Carolina near the contact between the Charlotte and Milton Belts of western North Carolina. More specifically, it is located in an area mapped as granitic rock and biotite gneiss and schist. Weathered rock recovered from our borings and exposed boulders exhibits the characteristics of biotite gneiss and is generally fine to medium grained. Soils weathered from the parent rock generally consist of silty, fine to coarse sands.

Existing NC 68 generally runs south-north and the elevation along the proposed centerline decreases from an elevation of approximately 837 feet at the beginning of the project to an elevation of approximately 805 feet near the existing culvert between East Harrell Road and West Harrell Road. The elevation then increases to an elevation of approximately 857 feet at the end of the project. Based on review of the cross sections provided, existing cuts appear to be on the order of approximately 10 to almost 30 feet on the south end of the project with the deepest cuts on the right side of the road. Existing embankment fills appear to be on the order of approximately 5 to 15 feet generally beginning near East Harrell Road and continuing northward, although none of the borings performed along NC 68 extended through the existing roadway embankment to verify this observation. It was noted during our preliminary site visit that isolated areas of minimally exposed rock were visible within the roadway shoulders towards the north end of the

project. What appeared to be an old road bed located parallel to and on the left/west side of NC 68, also contained boulders, although it appeared that they may have been placed during construction of this road. However, this area appears to be outside of the limits of the proposed construction.

The Haw River traverses the site in a generally east to west direction running beneath NC 68 through a box culvert located at approximate -L- station 23+70. Low-lying areas/flood plain with isolated area of wetlands (none located within the limits of the proposed construction) are present on either side of the river and appear to extend from East Harrell Road towards approximate -L- station 29+00.

The proposed alignment of East Harrell Road generally runs east-west and the elevation along the proposed centerline decreases from an elevation of approximately 822 feet at its intersection with NC 68 to an elevation of approximately 801 feet at its intersection with existing East Harrell Road. The topography along the proposed centerline is composed of three hills that will require cuts of up to approximately 28 feet and two low spots between the hills that will require fills of up to approximately 9 feet.

Soils Properties

Soils within this project area have been divided into three categories: topsoil, alluvial soils, and residual soils.

Topsoil: Topsoil was encountered at the surface of all of our borings and ranged in thickness from 0.1 to 0.3 feet (1 to 3.5 inches).

Alluvial Soil: Alluvial soils were encountered within the low-lying area at -Y1- station 13+50 and within the floodplain of the Haw River. The alluvial soil encountered at -Y1- station 13+50 consist of dark brown, fine sandy silt (A-4) with trace organics and man-made debris and some clay. The alluvial soil encountered within the floodplain of the Haw River typically consisted of silty and clayey, fine to coarse sand (A-2-4 & A-2-6) at -L- station 24+00 and intermixed layers of typically silty fine sand (A-2-4) and fine to coarse sandy and silty clay (A-7-5 & A-7-6) at -L- stations 23+00 and 27+00. The clay sample tested at boring L_2300R had a high plasticity index (LL=59, Pl=30). Trace organics were noted in the alluvial deposits. Based on the results of the hand auger borings, the consistency of the alluvial soils appears to be soft to stiff for the clay and very loose to medium dense for the sand. The soil moisture condition was typically moist to a depth of approximately 2 to 3 feet below the existing ground surface becoming wet or saturated at and below this depth.

Residual Soil: The majority of the soils encountered on the project are residual soils, and typically consist of silty fine to coarse sand (A-2-4), except at -L- stations 31+00 left and 35+07 right where surficial sandy and silty clays (A-7-5 & A-7-6) were encountered. The residual soil is generally red, brown and orange in color and contains trace organics near the existing ground surface. The tested sandy and silty soils are

either non-plastic or have low plasticity indices. The tested clay samples exhibit medium to high plasticity indices ranging from 17 to 32 percent and natural moisture contents ranging from 21 to 54 percent. The consistency of the residual soils ranges from very loose to very dense for the sands (most commonly medium dense to dense) and soft to very stiff for the clays (most commonly stiff).

Rock Properties

Both weathered rock and crystalline rock were encountered in the project corridor although crystalline rock was only encountered in two of the borings at -Y1- stations 11+50 and 19+50. The rock consists of brown, orange, white and black biotite gneiss. No rock coring was performed. At -Y1- station 11+50, layers of residual soil consisting of very dense silty, fine to coarse sand (A-2-4) were encountered within and below the weathered rock.

Groundwater Properties

Groundwater measurements were attempted at the time of drilling in all of the borings along -L-, but stabilized groundwater was not encountered with the exception of the boring located at station 27+00 where groundwater was encountered at an elevation of 790.4 feet, which is approximately 3 feet below proposed grade at the boring location or approximately 1.1 feet below proposed grade at the toe of the slope. The recovered soil samples were generally described as moist to wet, except the saturated alluvial soils encountered at Station 24+00 and 27+00.

Groundwater measurements were attempted in a majority of the borings along -Y1-, but stabilized groundwater was not encountered with the exception of the boring located at station 13+50 where groundwater was encountered at an elevation of 802.2 feet, which is approximately 9 feet below proposed grade. The recovered soil samples were generally described as moist.

Geotechnical Descriptive Analysis of the Project

For descriptive purposes, the project has been divided into four segments. The division of the segments is based on the topography and proposed roadway elevations.

-L- Station 13+90 to 22+50 (±):

This beginning of the project extends through an area with existing cut slopes typically ranging in height from approximately 10 to 30 feet. The widening will require additional cut depths up to approximately 13 feet with minimal to no additional cut required at the beginning and end of this segment. The unclassified excavation to be encountered in the additional cuts is anticipated to consist mainly of residual silty sands, weathered rock and crystalline rock.

Sheet 3B

-L- Station 22+50 to 29+00 (±):

This segment extends through the floodplain area of the Haw River with existing fill slopes typically ranging in height from approximately 5 to 15 feet. The widening will require additional fill depths up to approximately 8 feet or less which will extend into the floodplain (mainly on the right side of the road) where the groundwater elevation could rise to or above the existing ground surface elevation during wet periods.

-L- Station 29+00 to 39+50 (±):

This segment extends through the end of the project where the existing and proposed roadway is generally at or within a few feet of existing or proposed grades. The roadway subgrade is anticipated to consist of loose to medium dense silty and clayey sand (A-2-4 & A-2-6) and/or medium stiff to stiff silty clay (A-7-5 & A-7-6).

-Y1- Station 10+00 to 22+60 (±):

This segment consists of the entire alignment of the new roadway and contains proposed cut depths of up to approximately 28 feet and fill depths up to approximately 9 feet. The unclassified excavation to be encountered in the cuts is anticipated to consist mainly of dense to very dense silty sand (A-2-4) and weathered rock. The subgrade within the areas of proposed fill is anticipated to consist of medium stiff to stiff sandy silt (A-4) and loose to medium dense silty sand (A-2-4).

Sincerely,

FROEHLING & ROBERTSON, INC.

Geotechnical Engine

Daniel K. Schaefer, P.E. Raleigh Branch Manager

Earthwork Balance Sheet

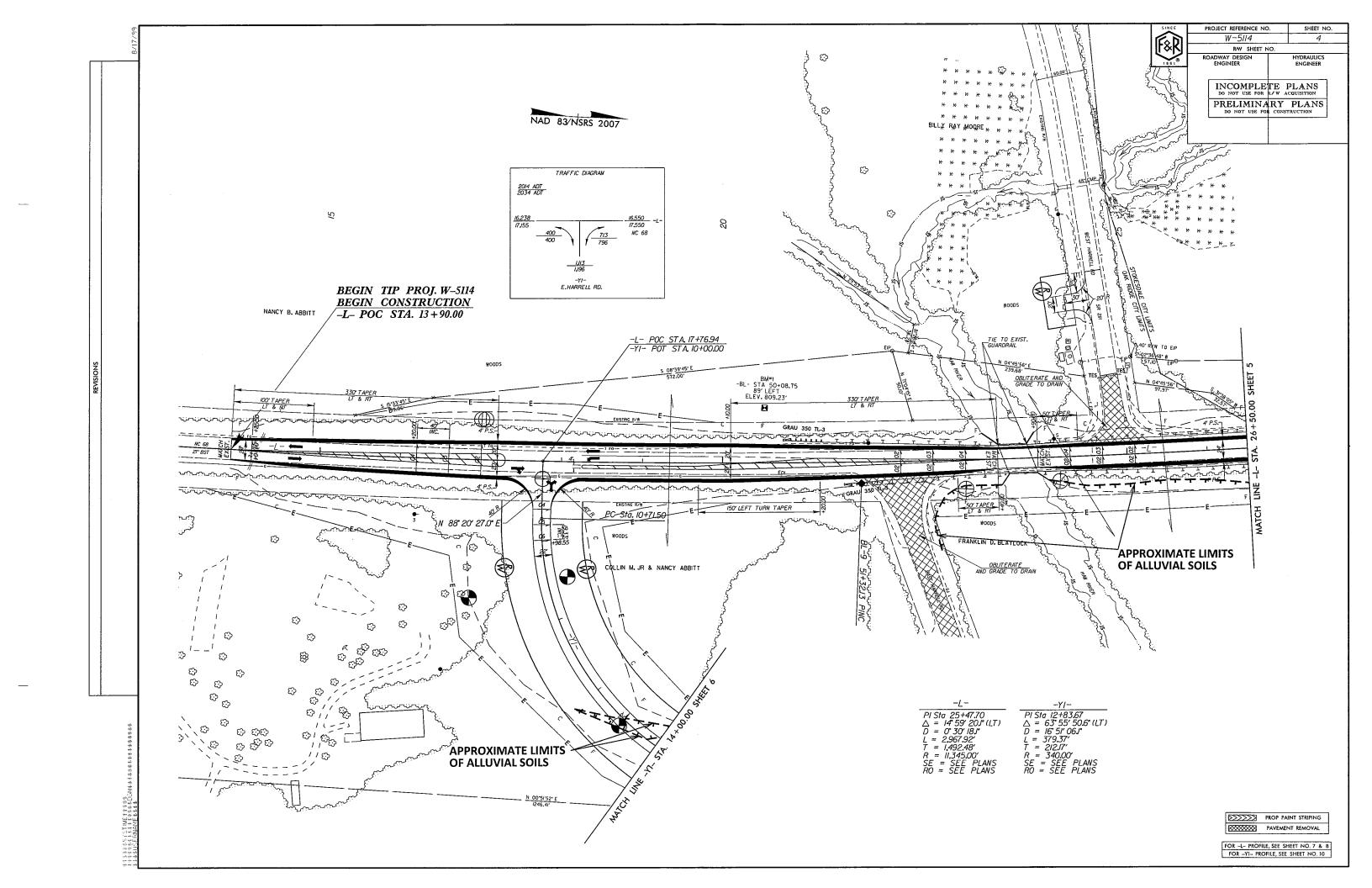
Volumes in Cubic Yards

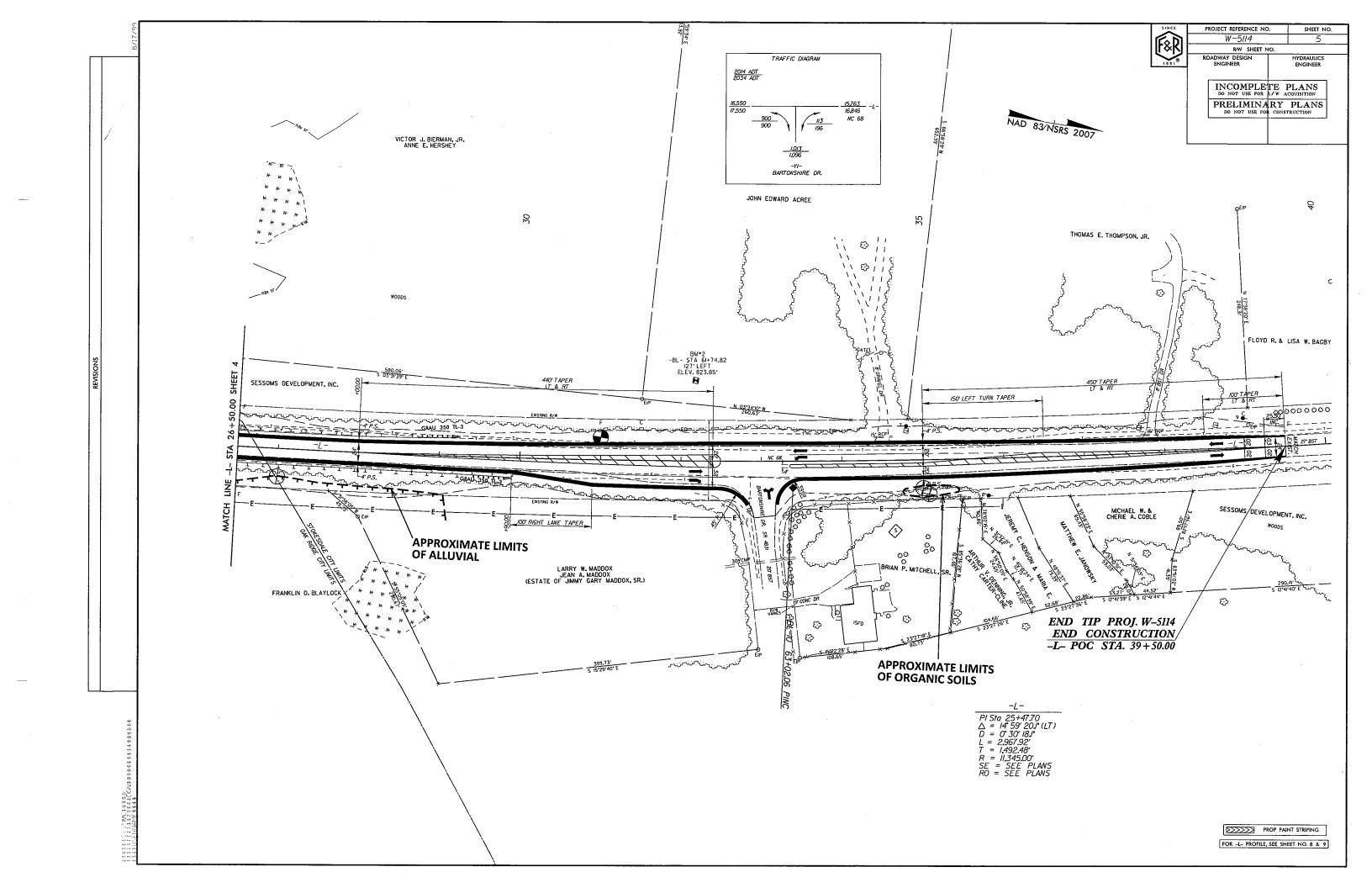
			cance in each run			
PROJECT: W-5114	COUNTY: Guilford	DATE:	1/15/2013	COMPILED BY:	JDM	SHEET 1 OF 1 SHEE
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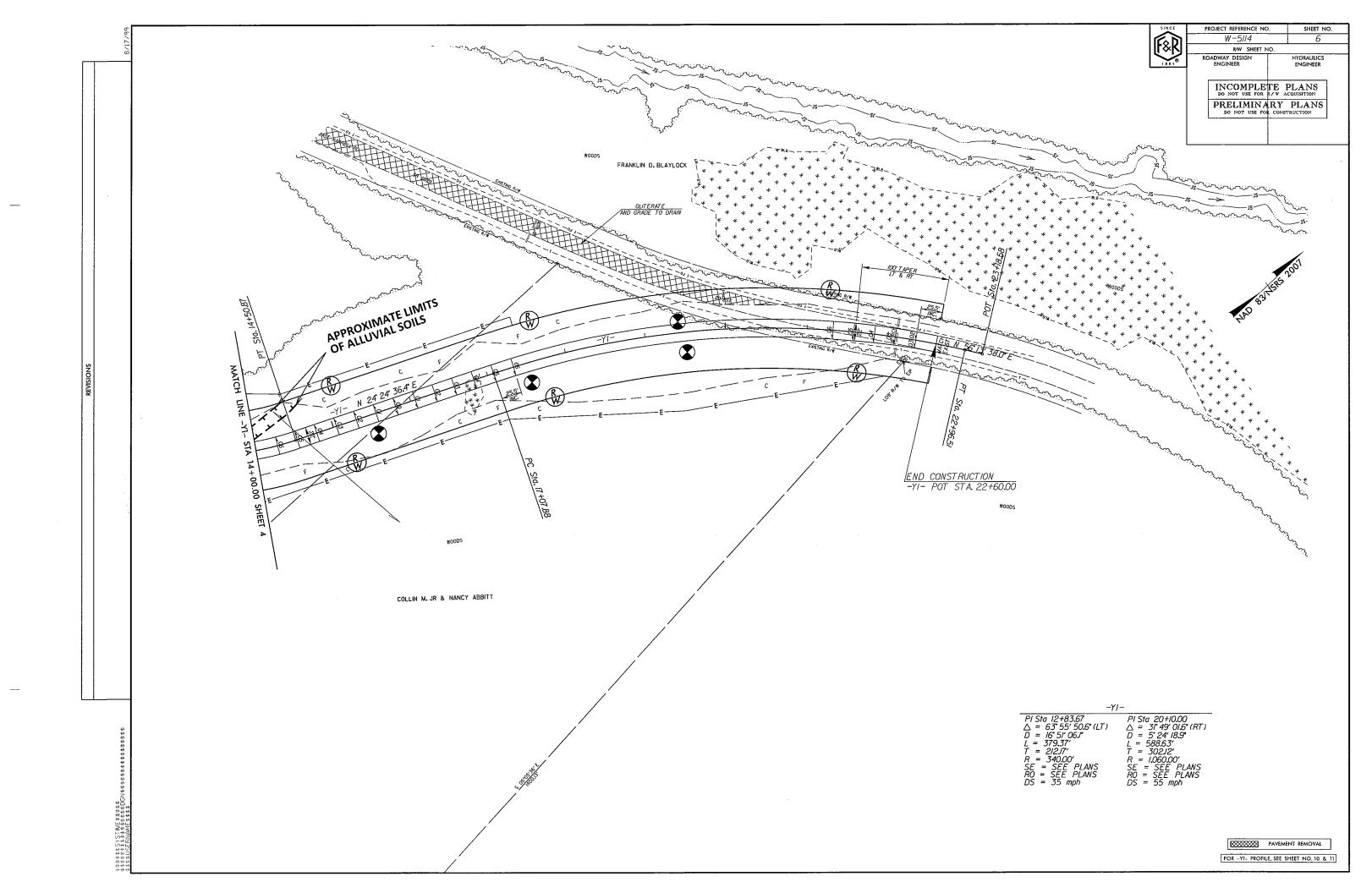
			l	EXCAVATIO	٧			EMBAN	KMENT			WASTE			
STATION	STATION	TOTAL	ROCK	UNDERCUT		SUITABLE	TOTAL	ROCK	EARTH	EMBANK.	BORROW	ROCK	SUITABLE	UNSUIT.	TOTAL
		UNCLASS.			UNCLASS.	UNCLASS.		<u>:</u> .		+20%					
-L- STA. 12+00.00 RT	-L- STA. 23+47.15 RT (CUL)	4,670			****	4,670	400		400	480	0		4,190		4,190
-L- STA. 13+90.00 LT	-L- STA. 23+47.15 LT (CUL)	1,959				1,959	373		373	448	0		1,511		1,511
						-									
					· · · · · · · · · · · · · · · · · · ·								7.701		
	SUBTOTAL	6,629				6,629	773		773	928	0		5,701		5,701
-L- STA. 23+83.21 RT (CUL)	-L- STA. 39+50.00 RT	128				128	3,348		3,348	4,018	3,890		0		0
-L- STA. 23+83.21 LT (CUL)	-L- STA. 39+50.00 LT	749				749	533		533	640	0		109		109
											·				
	SUBTOTAL	877				877	3,881		3,881	4,658	3,890		109		109
	SUBTOTILE						3,001		3,001	1,050	3,870		103		
-Y1- STA. 10+20.00	-Y1- STA. 22+60.00	33,198				33,198	2,092		2,092	2,510	0		30,688		30,688
	SUBTOTAL	33,198				33,198	2,092		2,092	2,510	0		30,688		30,688
Latenson															
														-	
TOTAL		40,704				40,704	6,746		6,746	8,096	3,890		36,498		36,498
IOIAL		40,704				40,704	0,740	,	0,740	0,090	3,890	<u> </u>	. 30,496		30,498
LOSS DUE TO CLEARING &	GRUBBING	-2,200				-2,200							-2,200		-2,200
WASTE IN LIEU OF BORRO											-3,890		-3,890		-3,890
GRAND TOTALS		38,504				38,504	6,746		6,746	8,096	0		30,408		30,408
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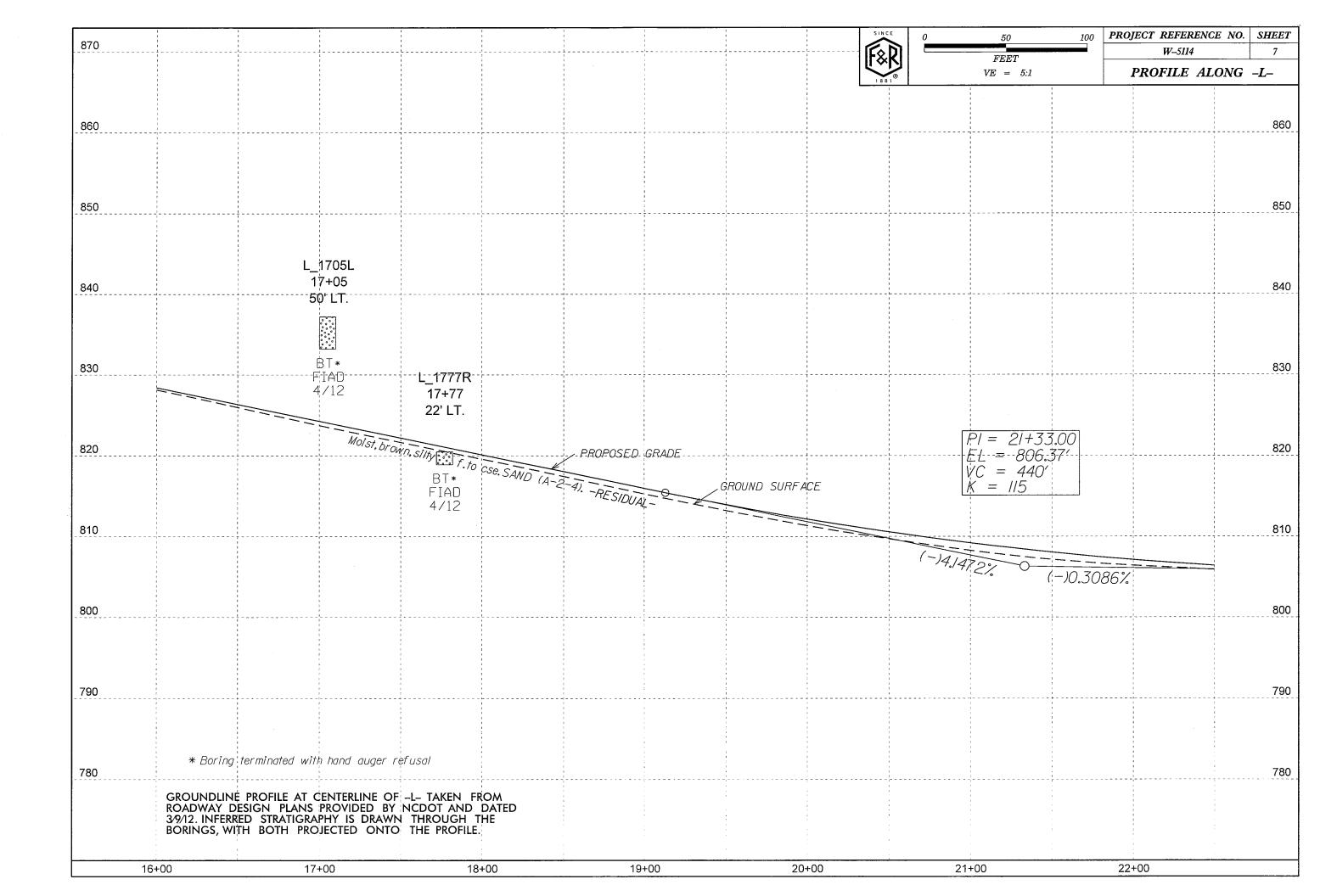
NOTE: EARTHWORK QUANTITIES ARE CALCULATED BY THE ROADWAY DESIGN UNIT. THESE EARTHWORK QUANTITIES ARE BASED IN PART ON SUBSURFACE DATA PROVIDED BY THE GEOTECHNICAL ENGINEERING UNIT.

ESTIMATED DDE = 410 C.Y.
ESTIMATED SHOULDER BORROW = 1,160 C.Y.
ESTIMATED UNDERCUT EXCAVATION = 1,300 C.Y.
ESTIMATED SELECT GRANULAR MATERIAL = 1,000 CY
PAVEMENT STRUCTURE VOLUME = 500 C. Y.

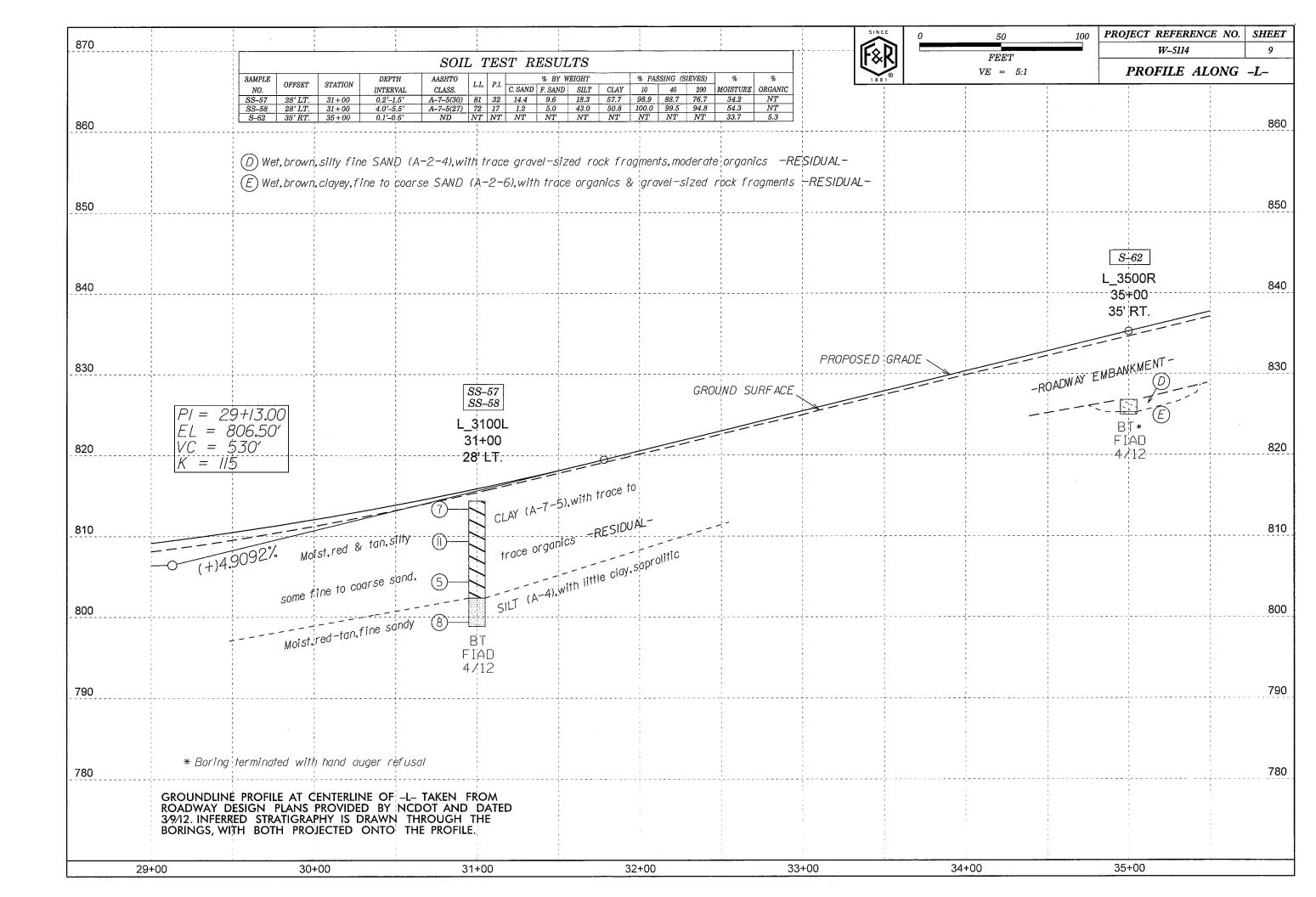


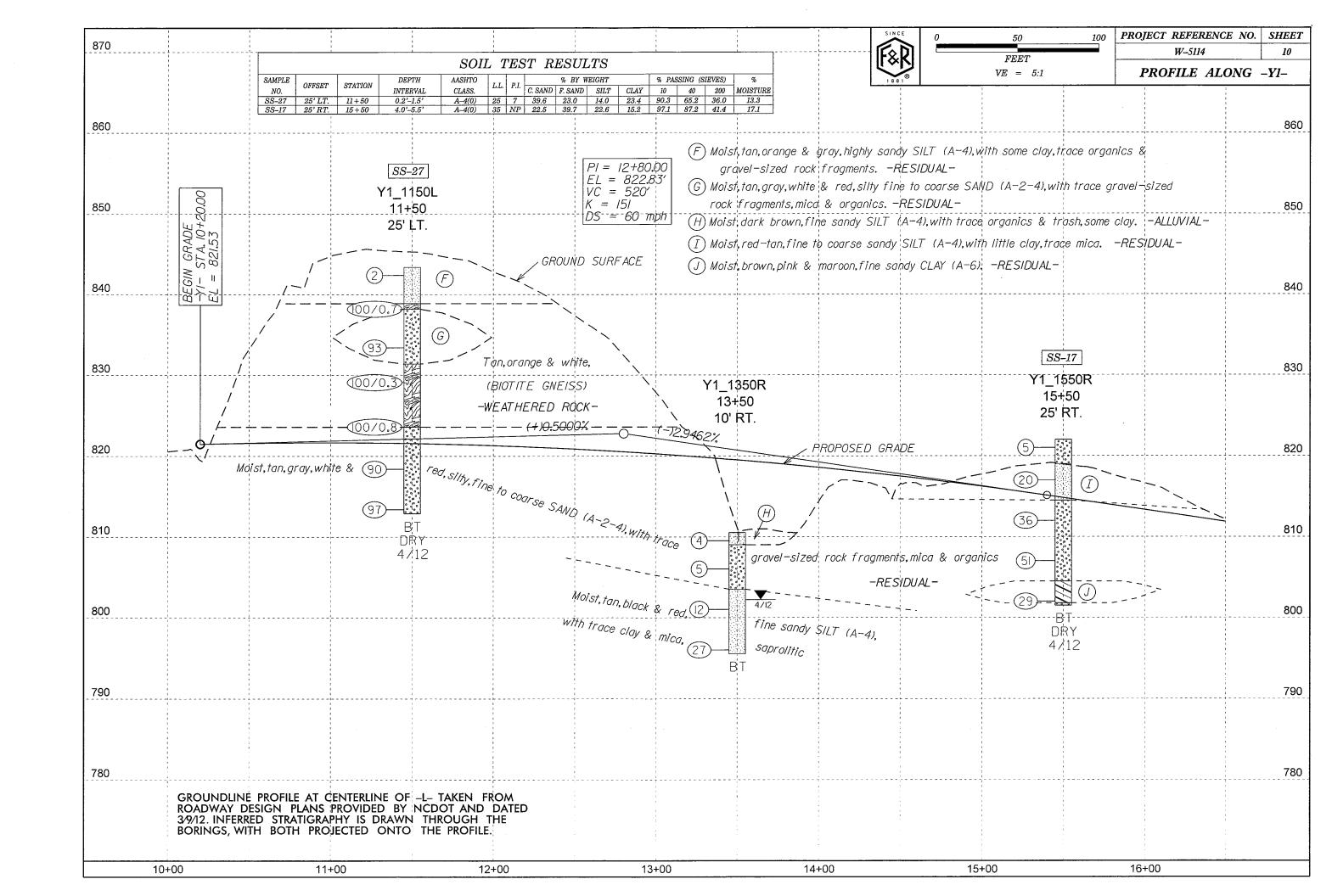


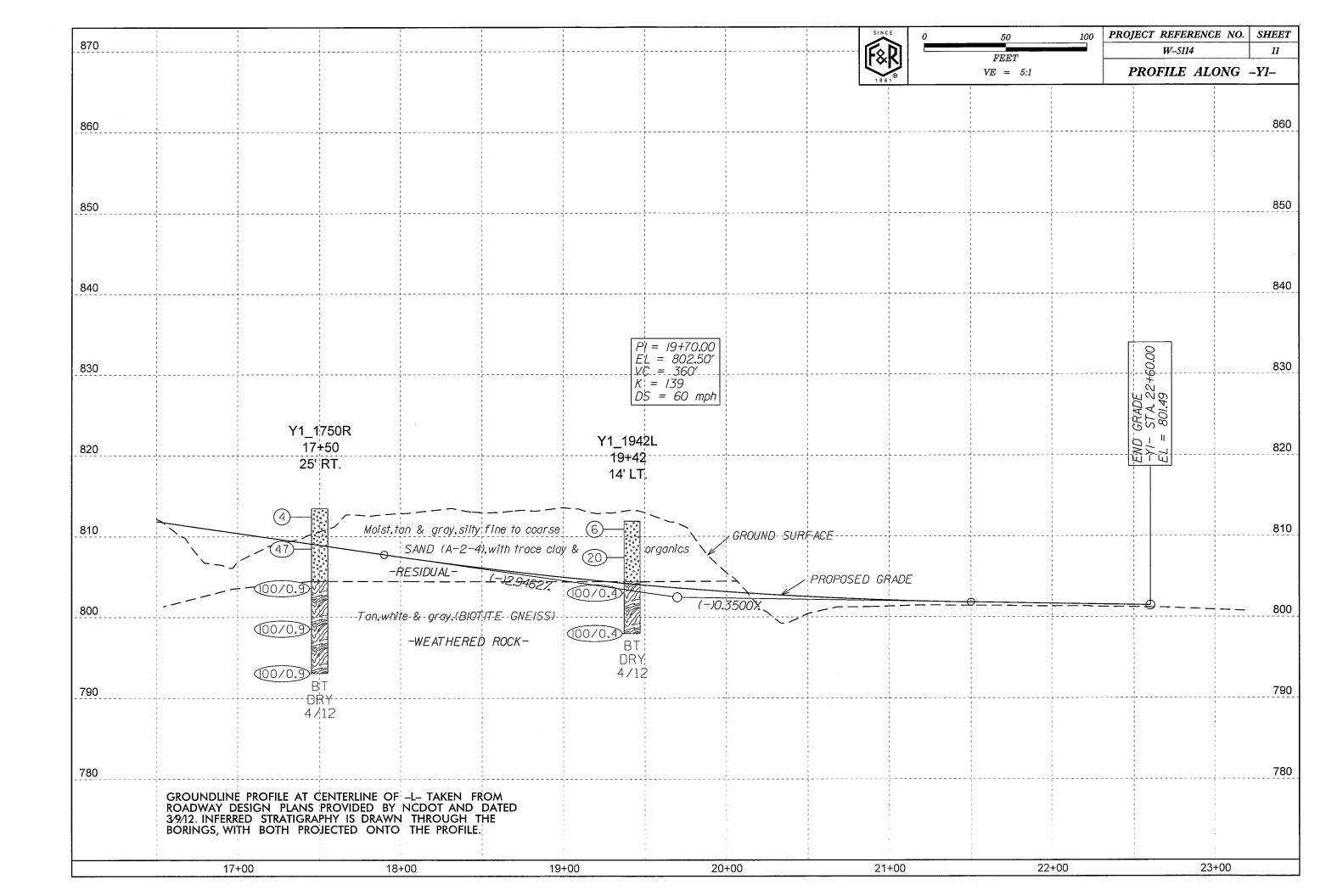


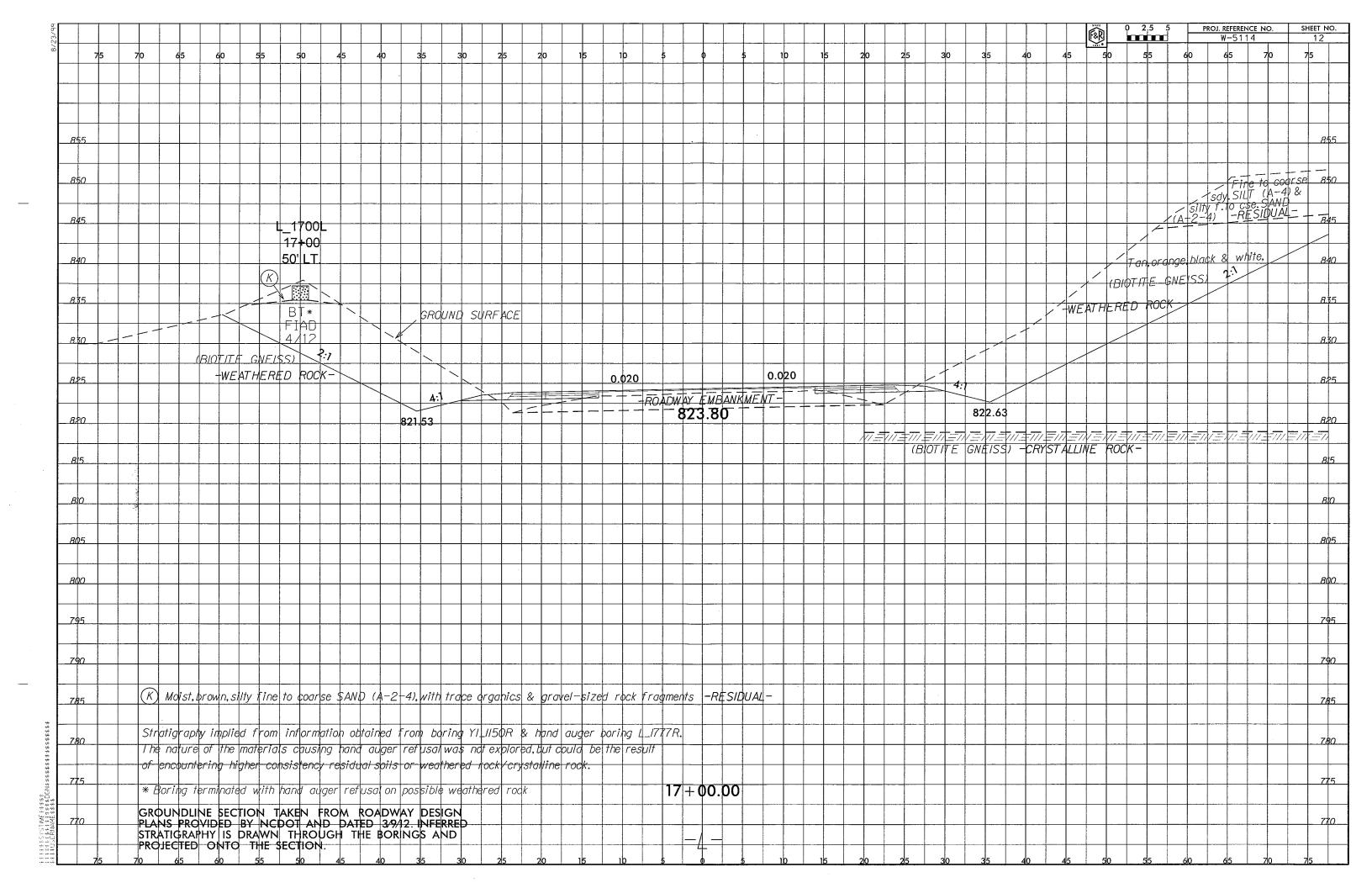


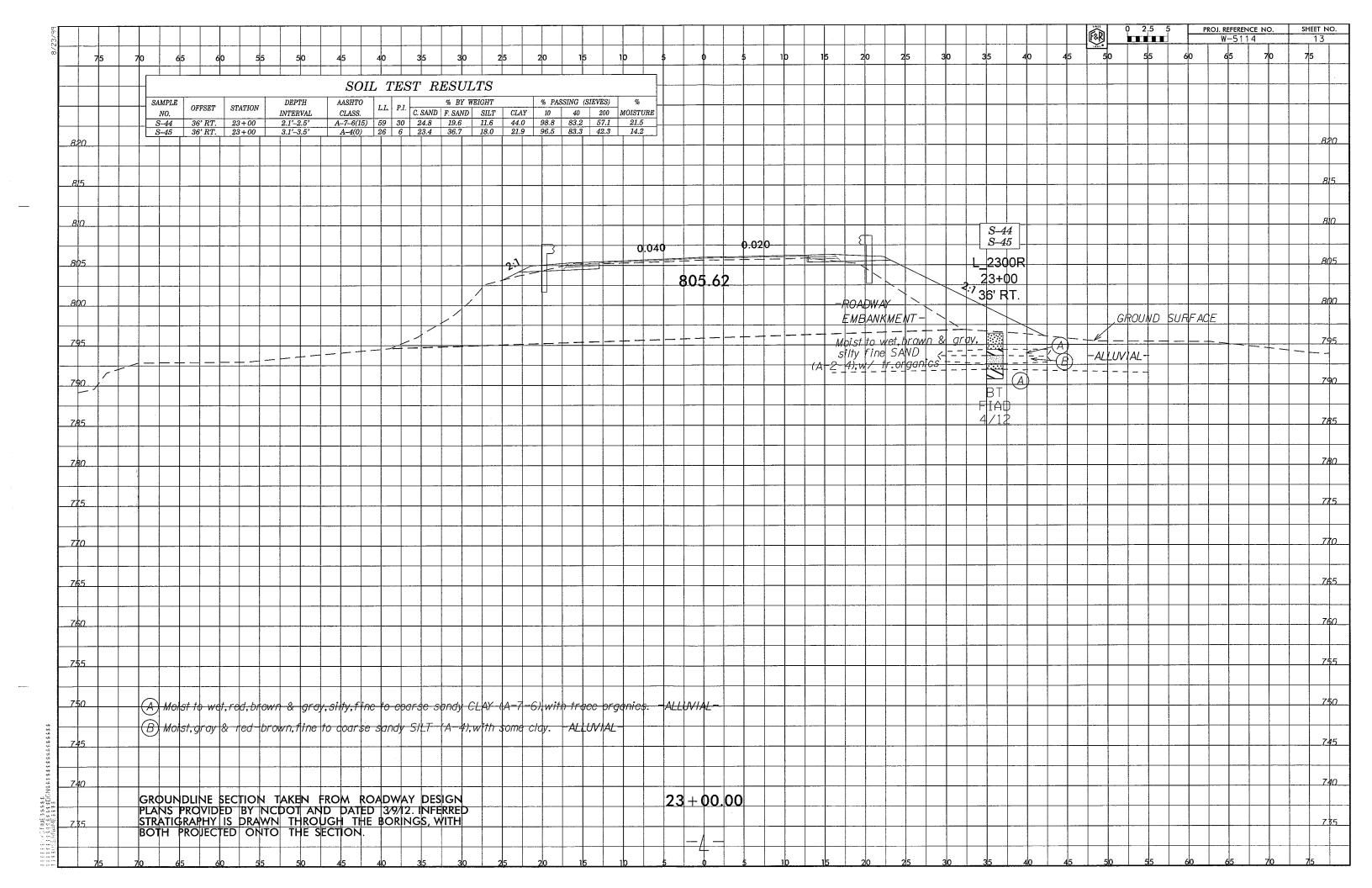
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		SAMPLE NO. S-44 36' I S-45 36' I	$\begin{array}{c cccc} ET & STATION & INTI- \\ \hline RT. & 23+00 & 2.1^2 \end{array}$	PTH AASHTO ERVAL CLASS.	L.L. P.I. C. SAND 5) 59 30 24.8	% BY WEIGHT F. SAND SILT CLA 19.6 11.6 44.	% PASSING (SIEVES) AY 10	0 MOISTURE .1 21.5		1881		VE = 5:1		PROFILE	ALONG	-L-
860				 	 	 	 	 				 	· - 			8
		A) Moist to	o wet,red,brown aray & red-brow	& gray,silty, n,fine to coal	fine to coarse se sandy SILT	sandy CLAY (A- (A-4),with sor	7-6),with trace ne clayALLUV	organicsA	LLUVIAL-			1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1				
850		C) Wet, bro	own,clayey fine t	o coarse SAN	D (A-2-6),wit	ἡ some silt. −A	\ <u>LLUVIAL</u> -	 	- 			: ! 	· - 			8
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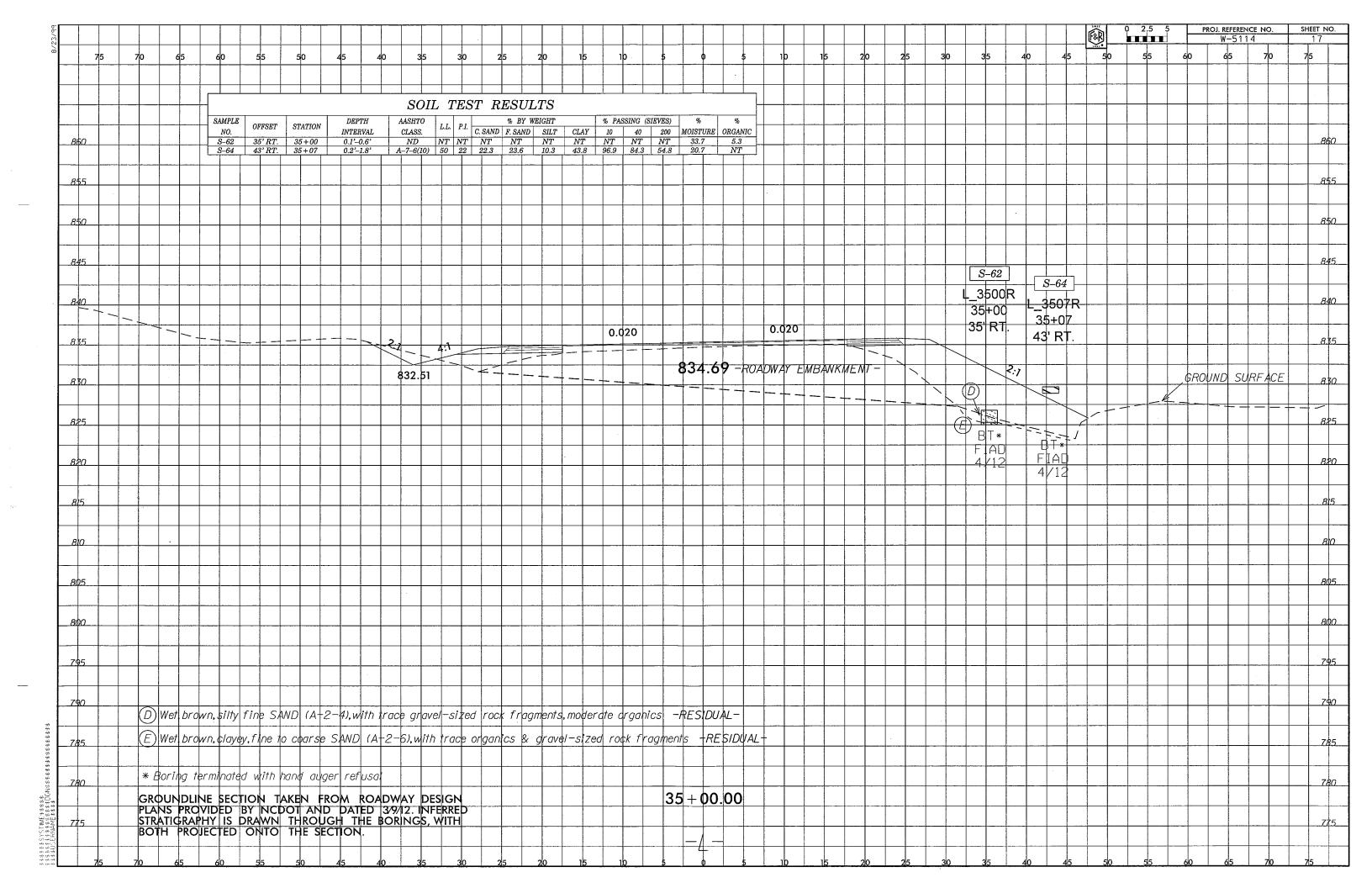


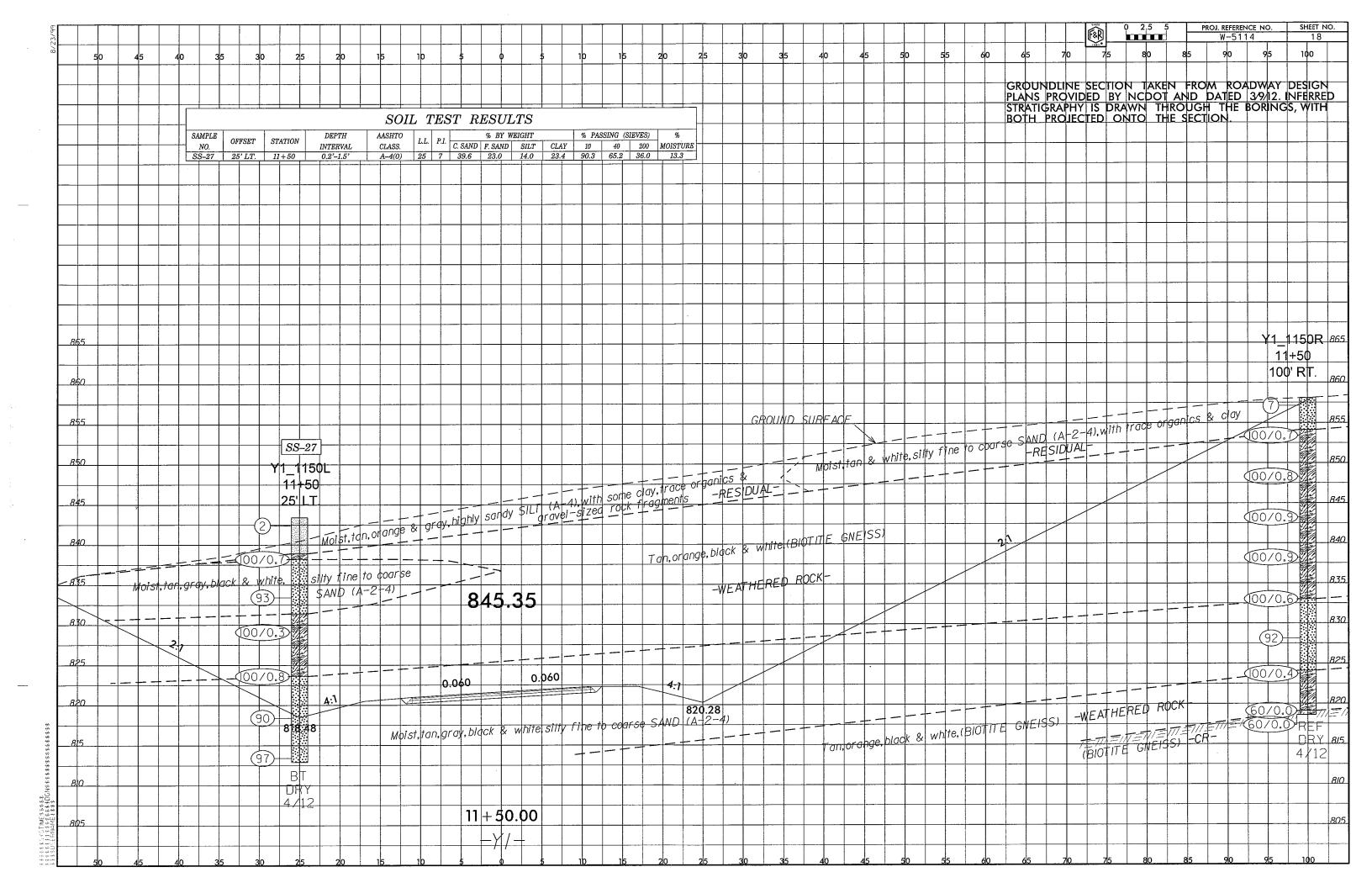


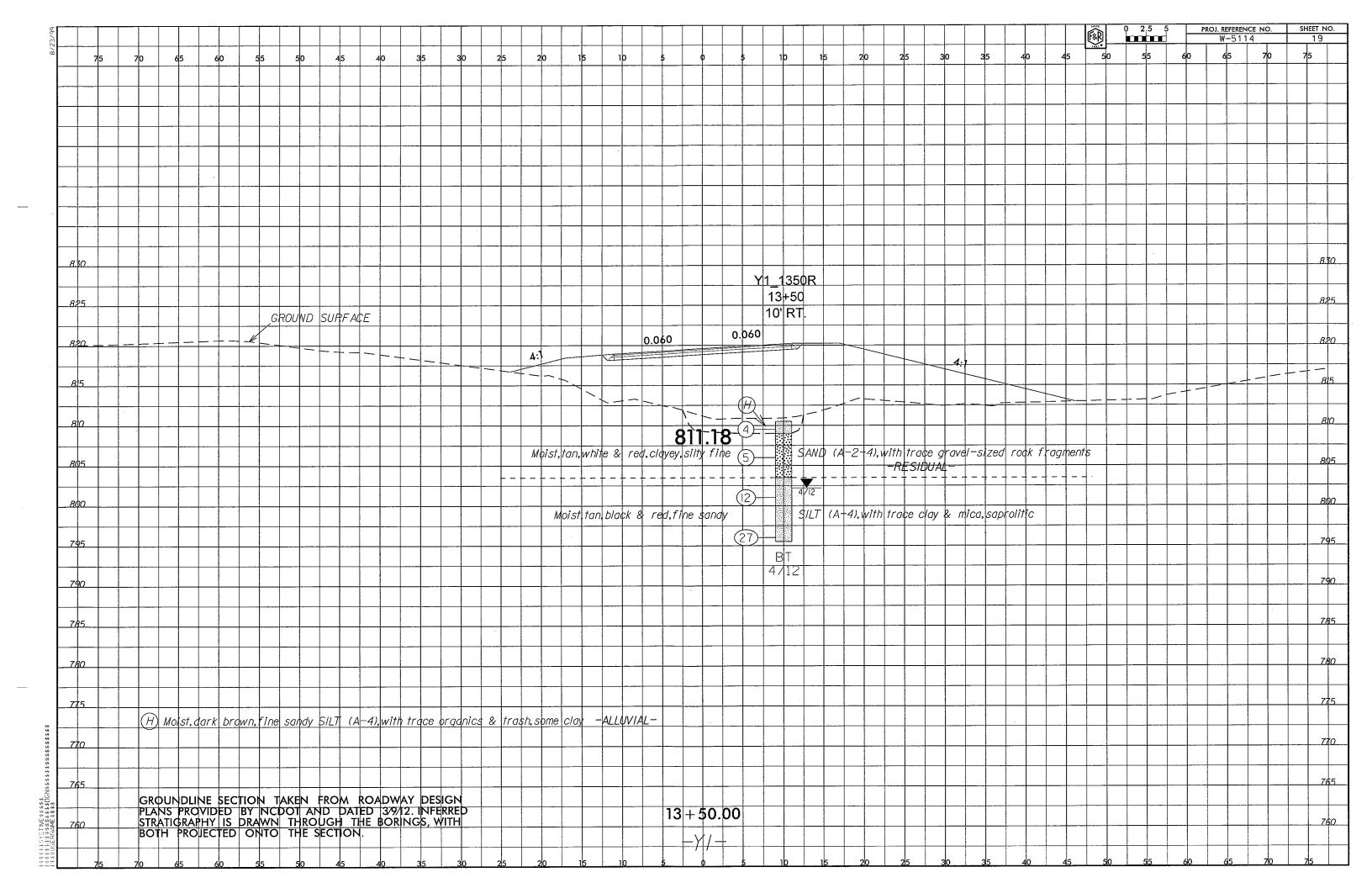


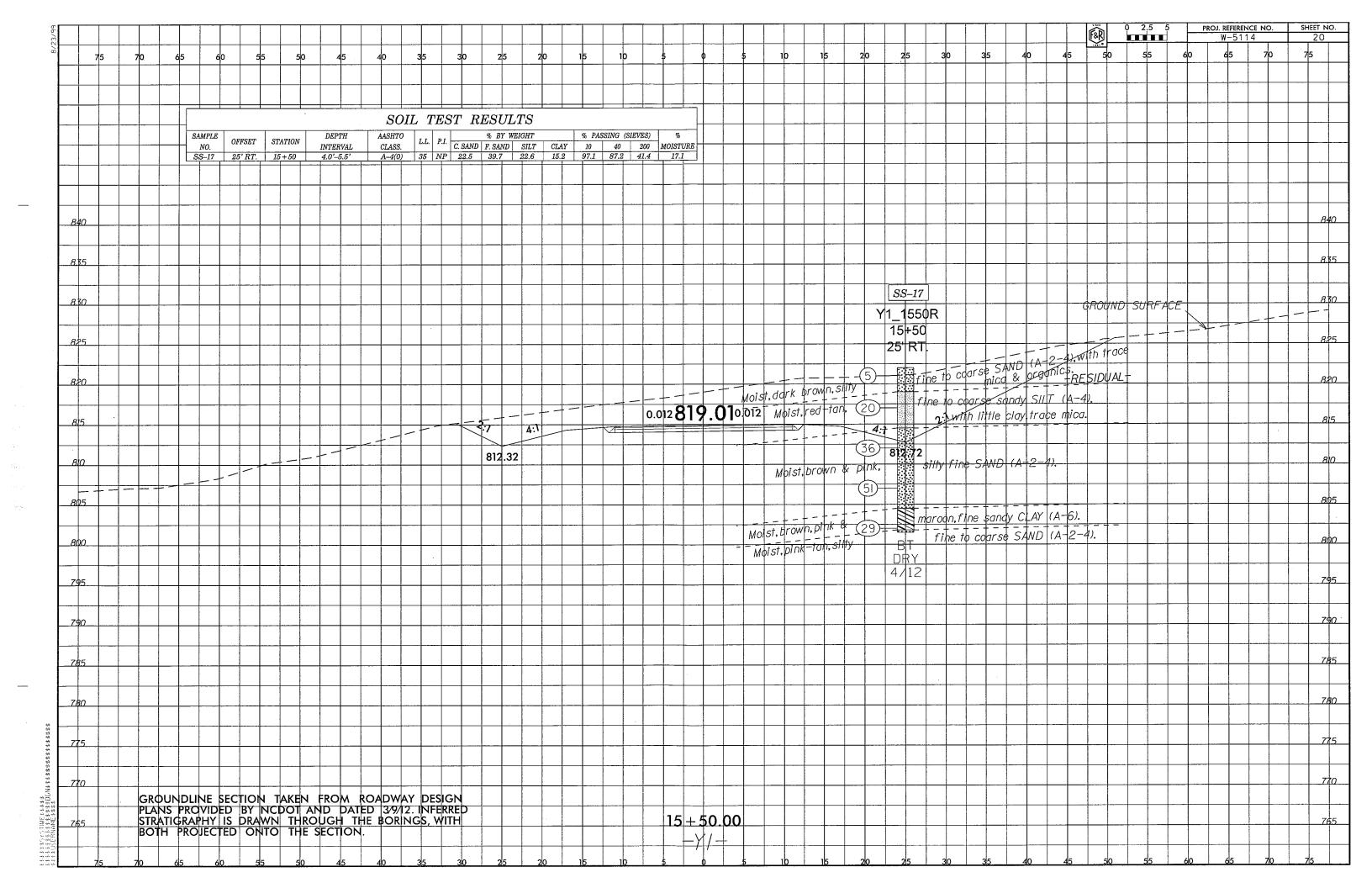


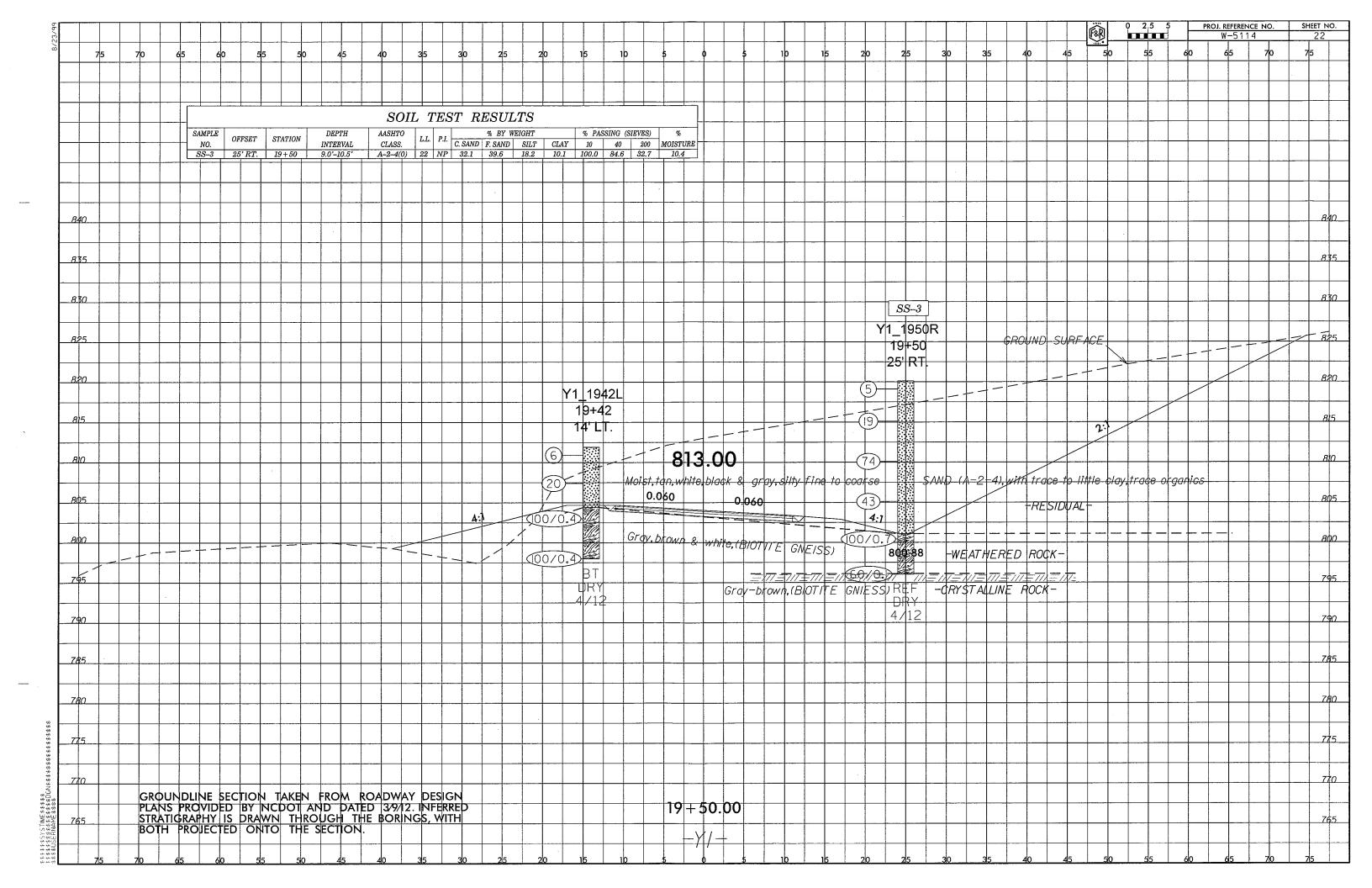












PROJECT NO.:

41877.1.1

TIP NO.:

W-5114

COUNTY:

Guilford

DESCRIPTION:

NC 68 from south of SR 2111 (East Harrell Road) to SR 4831 (Bartonshire Drive) in Oak Ridge and Stokesdale

Boring No.	Alignment	Station	Offset	Ground Surface Elevation (ft)	Test Depth* (ft)	Sample Blows (1.75" increments)		N _c	Termination			
					0	4	5	5	5			
L_1700L	-L-	17+00	50' LT	837.2	1.0	7	12	12	12	HAR @ 1.8'		
					1.8	25/0	_	-	25/0			
					2.2	11	18	17	17.5			
L_1705L	-L-	17+05	50' LT	837.2	3.0	14	18	22	20	HAR @ 4.0'		
					4.0	25/0	-	-	25/0			
L_1777R	-L-	17+77	22' RT	820.5	0	3	4	6	5	HAR @ 1.6'		
L_1///K		17177		820.5	1.0	16	20/0	-	20/0	HAK @ 1.6		
					0	3	3	6	4.5			
	-L-			796.4	1.0	8	8	11	9.5	HAT @ 5.7'		
L 2300R		23+00	36' RT		2.1	7	11	11	11			
L_2300K	_	25100			3.1	8	10	10	10			
					4.1	10	14	12	13			
					5.3	5	7	8	7.5			
					0	2	2	3	2.5			
					1.0	2	2	2	2			
L_2417R	-L-	24+17	30' RT	794.4	2.0	3	3	3	3	HAT @ 4.6'		
					3.2	2	2	3	2.5			
					4.1	3	3	3	3			
					0	4	5	4	4.5			
					1.0	4	5	5	5			
L_2700R	-L-	27+00	35' RT	792.7	2.0	4	4	3	3.5	HAT @ 5.4'		
L_2700K	-	27100	33 1(1	752.7	3.5	3	4	5	4.5	HAT @ 5.4		
					4.0	10	10	12	11			
					5.0	7	8	10	9			
					0	2	3	4	3.5			
L_3500R	-L-	35+00	35+00	35' RT	826.8	1.0	7	12	8	10	HAR @ 1.8'	
					1.8	20/0	-	-	20/0			
L_3507R	-L-	35+07	43' RT	829.7	_	-	-	-		HAR @ 0.8'		

DCP Testing was performed in accordance with ASTM Special Technical Publication No. 399

HAT = Hand Auger Terminated

HAR = Hand Auger Refusal

^{*}Test depth referenced from existing ground surface